

U.S. Army Corps of Engineers

New England District Concord, Massachusetts

SUPPLEMENTAL DESIGN INFORMATION FOR THE PHASE 1/PHASE 2 TRANSITION AREA OF THE 1.5-MILE REACH REMOVAL ACTION

DCN: GE-062703-ABRG

June 27, 2003

Site-Specific Environmental Remediation Contract General Electric (GE)/Housatonic River Project Pittsfield, Massachusetts

Contract No. DACW33-00-D-0006
Task Order No. 0005

02M-0140



GE-062 703-ABBG

United States Environmental Protection Agency EPA New England One Congress Street, Suite 1100 Boston, MA 02114-2023

June 27, 2003

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Public Information Repositories

RE: Transmittal of the Final Plans, Specifications, and Supplemental Design Information for the Phase 1/Phase 2 Transition Area 1.5 Mile Reach Removal Action GE-Pittsfield/Housatonic River Site, Pittsfield, Massachusetts

Enclosed please find the following:

- Final Specifications for the Phase 1/Phase 2 Transition Area of the 1.5 Mile Removal Action, by Weston Solutions, April 2003 (PD)
- Final Design Submittal Drawings, Phase 1/Phase 2 Transition
- Supplemental Design Information for the Phase 1/Phase 2 Transition Area of the 1.5 Mile Reach Removal Action, by Weston Solutions, June 27, 2003 (PBR 4)

The Phase 1/Phase 2 Transition Area of the 1.5 Mile Removal Action encompasses approximately 750 feet from the end of the Phase 1 to the Elm Street bridge. Also included in the plans and specifications is the gravity bypass dam and piping system. The supplemental design information includes the following: amendments to the final drawings and specifications; summary tables regarding excavation volumes, backfill volumes, TSCA and non-TSCA volumes, and changes in flood storage capacity; and information on the projected impacts of the construction during high flow events.

If you have any questions, please contact me at (413) 236-0969.

Sincerely,

Dean Tagliaferro

Enclosures

This document provides supplemental information prepared as part of the finalization of the Phase 1/Phase 2 Transition Area design. The paragraphs below provide a brief description of the information, and pertinent tables and figures are included as Attachments to this document. The three main elements presented in this document are as follows:

- Amendments to the Final Drawings and Specifications
- Tables listing excavation and backfill volumes and associated flood storage changes for the Transition Phase and for the Lyman to Elm Street reach of the 1.5 Mile Reach. The Lyman to Elm Street reach encompasses Phase 1 and the Phase 1/Phase 2 Transition Area of the 1.5 Mile Reach.
- Documentation of the HEC-RAS Model results for Lyman to Elm Street

Amendments to the Design

Based on additional comments provided by the Army Corps of Engineers (ACOE) and USEPA, Weston has provided a list of Amendments to the Transition Phase Specifications and Drawings. These Amendments are included in Attachment A to this document. There are a total of 28 amendments to the design, mostly editorial in nature.

Final Excavation and Backfill Volumes

Weston conducted analysis and calculations relative to the excavation and backfill amounts and resulting flood storage capacity changes based on the final design for the Transition Phase. The results of the calculations are provided in Attachment B in the form of two sets of four tables for the Transition Area and for the Lyman Street to Elm Street Reach, respectively. These tables are as follows:

Table B-1	Final Transition Area Design Excavation and Backfill Volumes
Table B-2	Final Transition Area Design Excavation Volumes by Soil/Sediment
	Classification
Table B-3	Summary of Estimated Flood Storage Capacity Changes for Transition
	Reach
Table B-4	Comparison of Excavation Volume Estimates in Cubic Yards for
	Transition Area
Table B-5	Design Excavation and Backfill Volumes – Lyman to Elm
Table B-6	Design Excavation Volumes by Soil/Sediment Classification – Lyman
	to Elm
Table B-7	Summary of Estimated Flood Storage Capacity Changes – Lyman to Elm
Table B-8	Comparison of Excavation Volume Estimates in Cubic Yards for Lyman
	to Elm Street Area

Based on the calculations and as documented in the tables in Attachment B, the total amount of flood storage capacity gain in the Transition Area is 700 cubic yards, and the total amount of flood storage capacity gain from Lyman to Elm Streets is 1,900 cubic yards.

HEC RAS Model Results

Summarized below and in Attachment C are the updated results of the HEC-RAS modeling based on input of the final design cross-sections for the Transition Phase. Below is a summary of the results and conclusions derived from the modeling. Note that these results and the documentation below will be incorporated into the Draft Final Basis of Design document for Phase II.

HEC-RAS Model Input Changes

New cross-section geometry was updated in April 2003. The new geometry was entered into the HEC-RAS model for transition area stations 514+00 through 521+00. Due to the new retaining wall scheme (varying riprap sizes for the channel and bank, and vegetative cover beyond the river bank armor), the Manning's 'n' roughness coefficients were changed accordingly. These changes were dictated by the notes provided on the Drawings: Existing and Proposed Riverbank Cross-Sections, Sheets 1 and 2 (Sheet reference numbers 2008 and 2009). The Manning's 'n' value formula used for channel and lower bank design conditions is as follows:

$$n = y^{1/6} / [21.6 \log_{10}(y/d_{50}) + 14]$$

where y = depth of flow (ft) and d_{50} = riprap size (ft)

The depths of flow vary from station to station throughout the transition area. They were approximated from the existing model output during the 10-yr design storm. Three different riprap sizes are used in the transition area, 9-in, 12-in, and-18 in. On all cross-sections within the transition area, 18-in riprap is used for the 1:1 sheet-pile wall covering and the areas from the edge of river up to the vegetative cover. This resulted in Manning's n values of 0.037 to 0.045 for the Transition Area (Station 514+00 to the Elm St. bridge) for the lower banks and channel. Note that the Manning's value used for the channel from Stations 500+00 to 514+00 (Phase 1) was 0.033 for the design condition. The Manning's value for the post-construction vegetative cover (design conditions) is generally the same as for existing conditions. This is based on eventual re-establishment of trees and vegetation. Manning's values used for overbank and floodplain areas range from 0.02 to 0.1, and were not changed from existing to design conditions. Existing conditions in these areas range from paved areas to heavily wooded/brush areas. The Manning's values used are considered reasonably conservative for the final restored river channel configuration

HEC-RAS Model Results Summary

The HEC-RAS model water surface elevation results were evaluated from Construction Stations 500+00 through 521+00 (Lyman Street to Elm Street). A tabular summary of the model results is provided in Table C-1. Four sets of two model output figures are also provided depicting flood stage heights for the 100, 50, 10 and 5-year storms. For each storm, one figure shows existing conditions versus design condition flood stage height, and the second figure shows design condition flood stage height versus top of bank elevations.

The modeling results for Lyman Street to Elm Street show that the implementation of the removal action as designed will not significantly alter flood elevations or river flow velocities in this reach. The maximum increase in river flow velocity is 1.01 ft/sec during the 10-year storm event (4,375 cfs) at Station 506+00 (increase from 4 to 5 ft/sec). The maximum increase in water surface elevation is 0.38 ft. at Station 519+50, and occurs during the 10-yr storm event (4,375 cfs) and within approximately 200 ft. upstream of the Elm St. bridge. The maximum water surface elevation increase at Lyman Street (Station 500+00) is 0.14 feet, also during the 10-yr storm.

Attachment A

Final Specifications and Drawings for the Phase 1/Phase 2 Transition Area 1.5 Mile Reach Removal Action

I. Amendments to Specifications

Specification Section 01025 – MEASUREMENT AND PAYMENT

1. In the last sentence of Paragraph 1.1.5b, "River Diversion System Gravity Operation," replace the word "pumping" with "gravity."

Specification Section 01330 - SUBMITTAL PROCEDURES

- 2. On page 3 of 3 of the Submittal Register (attached table), Item 103, under "Description of Item Submitted," correct spelling to "structure" instead of "struction."
- 3. Add to Submittal Register, submittals for slide gates and pipe as indicated in items 15 and 18 below.

Specification Section 02300 - EARTHWORK

- 5. Delete the reference to ASTM C 33 under Paragraph 1.1 "References."
- 6. Paragraph 2.3, delete "ASTM C33" and replace with "the State Specifications for Highways and Bridges".

<u>Specification Section 02370 – STORMWATER AND EROSION CONTROL:</u> IN-RIVER WORK

7. On Page 02370-20, Subsection 3.3.2.3 "Monitoring to Anticipate a Flood Event," change the first sentence in paragraph a as follows: after "Gaging Station" add "corrected for the site's downstream location" and after "maximum flow" add "(estimated at approximately 180 cfs)."

Specification Section 11000, HOUSATONIC RIVER BYPASS GRAVITY FLOW SYSTEM

- 8. In Paragraph 1.2b, change "electric" to "manual" in item 3.
- 9. In subsection 2.1, paragraph g, change the sentence as follows: "...the Pre-Design Document and Basis of Design Document for Phase 2."
- 10. Change last bullet under Paragraph 2.1, part I, to "Net force of zero applied to connection with conveyance piping at dam."
- 11. Under Paragraph 2.1 item k, at the end of the first sentence, add the following, "or one inlet structure covering both gravity intakes. In either case, each inlet structure

must allow for raising and lowering of the slide gates individually or must be easily removed for lowering of the slide gates."

- 12. Under Paragraph 2.2, at end of first sentence, remove the word "intake."
- 13. In Paragraph 3.2, beneath the bullets under item no. 2, add the following "In addition, installation shall conform with appropriate ASTM standards as referenced by the above PPI standards (see also Specification Section 15064 PLASTIC PIPE, paragraph 2.2.)"
- 14. At the end of paragraph 3.2, add no. 7: "Flanged connnections must be installed per the manufacturers instructions. The two pipes being joined via flanges shall be in full contact at the joining edge prior to tightening of the flange bolts. In no instances shall the flanged fittings and bolts be used to pull two pieces of pipe together."

Specification Section 11160 – SLIDE GATES

15. Add Paragraph 1.2 Submittals and include:

Submit under the provisions of Section 01330.

SD-02 Shop Drawings

Include dimensions and details of construction of slide gates, operators and appurtenances proposed for use.

SD-10 Operation and Maintenance Data

Operation and maintenance manuals shall be submitted with or before delivery of the slide gates to the site.

- 16. Under Part 3 Execution, delete section 3.1 Submittals.
- 17. Under Section 3.2, Installation, the text should read "Slide gates and operators shall be installed per manufacturer's instructions."

Specification Section 11800 - WATER TREATMENT SYSTEM

18. Modify the last sentence in Section 1.1, "System Overview" to the following: "It does not include conveyance piping from the discharge of the excavation dewatering system to the treatment system and other components of the dewatering system as required by Specification Section 02300, "EARTHWORK."

Specification Section 15064 - PLASTIC PIPE

19. Insert new paragraph 1.3 Submittals and include:

SD-03 Product Data

Submit manufacturer's product data for pipe and fittings including materials of construction, dimensions and physical characteristics.

SD-06 Test Reports

Submit information pertaining to making each fusion weld including: ambient weather conditions (temperature, wind speed, cloud cover and precipitation), operator's name, current certificate qualifying the operator to operate the fusion equipment used, pressure applied, time of applied pressure and temperature of joint during the fusion process.

SD-07 Certificates

Training certificates of personnel performing fusion welding shall be submitted prior to any fusion welding. Certificates shall qualify each operator to operate the fusion equipment used.

SD-08 Manufacturer's Instructions

Submit manufacturer's design, installation, handling, joining and maintenance instructions.

20. Add the following to paragraph 2.1 GENERAL: after "ASTM" add "and PPI".

II. Amendments to Drawings

<u>Sheet 2001 – TRANSITION AREA RETAINING WALL SECTIONS AND ARMOR</u> DETAILS

21. At each detail, add "(left)" and "(right)" next to all instances of "east" and "west" banks.

Sheet 2003 – DIVERSION DAM ELEVATION

22. Add the following note to east and west sides at existing ground surface elevation 976 feet: "Sheetpile shall be extended 25 feet into bank beyond existing ground surface elevation 976 feet. See also Sheet 2002."

23. Delete Note 1.

Sheet 2004 – DIVERSION DAM DETAILS 1

- 24. Change 2' 0" vertical dimension in Section A indicating sheetpile penetration includes pile cap to 1' 6".
- 25. Sections A and B, change note at middle right to "ALL PIER BRACING \bot S 3 1/2 x 3 1/2 x 1/4 CONNECTION AT INTERSECTION."

Sheet 2005 – DIVERSION DAM WALKWAY PLAN AND DETAILS SHEET 1 OF 2

- 26. In the upper left of the sheet (Walkway Plan), the 10" dimension should be corrected to 9" and the 1'0" dimension should be corrected to 1'1".
- 27. Note 2 under "WALKWAY PLAN" should read as follows: "ALL HORIZONTAL X-BRACING $\ ^{\rm S}$ 2 1/2 x 2 1/2 x 1/4."

Sheet 2007 – EXISTING AND PROPOSED RIVERBANK CROSS SECTIONS SHEET 1 OF 2

28. Add note immediately below "Armor Elevations" to state the following: "Upper elevation of riverbed armor shall be 971 feet."



Table B-1 - Final Transition Area (Station 514+00 to Elm St.) Design Excavation and Backfill Volumes

Ì	Cut (CY)	Fill (CY)
East Bank	1,900	2,000
River Bed	5,400	4,500
West Bank	1,900	2,000
Total	9,200	8,500
Overexcavation (@10%)	900	900
Total (w/ overexcavation)	10,100	9,400

Table B-2 - Final Transition Area (Station 514+00 to Elm St.) Design Excavation Volumes by Soil/Sediment Classification

Soil/Sediment Classification	In-Place Volume	Total With Overexcavation Factor of 10%
Bank Soil (TSCA)	900	1,000
Riverbed (TSCA)	700	800
Total TSCA	1,600	1,800
non-TSCA	7,600	8,300
Total	9,200	10,100

Table B-3
Summary of Estimated Flood Storage Capacity (FSC) Changes for Transition Reach
(Station 514+00 to Elm St.)

Section	Volume in cubic yards ¹
Volume of Material to be Excavated	10,100
Volume of Material to be Backfilled	(9,400)
Net Change between the Existing Conditions and	
the Final Transition Area Design	
Excavation/Backfilling	700

Positive value indicates net increase and negative value indicates loss.

Table B-4
Comparison of Excavation Volume Estimates in Cubic Yards
(in-place volume) for Transition Area (Station 514+00 to Elm St.)

Location	EE/CA	Final Design Calculation
East Bank	1,700	1,900
River	5,500	5,400
West Bank	3,000	1,900
Total (in place)	10,200	9,200
Total with 10% Overexcavation Factor	11,200	10,100

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Table B-5
Design Excavation and Backfill Volumes
Lyman to Elm

[Lyman	to 514+00	514+0	0 to Elm	Lyman to Elm		
	Cut (CY)	Fill (CY)	Cut (CY)	Fill (CY)	Cut (CY)	Fill (CY)	
East Bank	5,200	5,000	1,900	2,000	7,100	7,000	
River Bed	8,200	7,300	5,400	4,500	13,600	11,800	
West Bank	4,500	4,400	1,900	2,000	6,400	6,400	
Total	17,900	16,700	9,200	8,500	27,100	25,200	
Overexcavation (@10%)	1,800	1,800	900	900	2,700	2,700	
Total (w/ overexcavation)	19,700	18,500	10,100	9,400	29,800	27,900	

Note: Fill volumes for the Lyman St. to Elm St. reach represent corrected values. A 200 cy error was discovered in the Phase 1 BOD report.

Table B-6
Final Design Excavation Volumes by Soil/Sediment Classification
Lyman to Elm

	Lyman to	Station 514+00	Station 51	4+00 to Elm St.	Lyman St. to Elm St.		
Soil/Sediment Classification	In-Place Volume	Total With Overexcavation Factor of 10%	In-Place Volume	Total With Overexcavation Factor of 10%	In-Place Volume	Total With Overexcavation Factor of 10%	
Total TSCA Material	2,900	3,200	1,600	1,800	4,500	5,000	
non-TSCA	15,000	16,500	7,600	8,300	22,600	24,800	
Total	17,900	19,700	9,200	10,100	27,100	29,800	

Table B-7 Summary of Estimated Flood Storage Capacity (FSC) Changes
Lyman to Elm

		Volume in cubic yards ¹	
	Lyman to 514+00	514+00 to Elm	Lyman to Elm
Volume of Material to be Excavated	19,700	10,100	29,800
Volume of Material to be Backfilled	(18,500)	(9,400)	(27,900)
Net Increase in Flood Storage			
Capacity	1,200	700	1,900

^{1.} Positive value indicates net increase and negative value indicates loss.

Table B-8
Comparison of Excavation Volume Estimates in Cubic Yards (in-place volume) for Lyman to Elm Street Area

	Volume in cubic yards									
	Lyma	n to 514+00	514+	·00 to Elm	Lyman to Elm					
Location	EE/CA	Final Design Calculation	EE/CA	Final Design Calculation	EE/CA	Final Design Calculation				
East Bank	4,200	5,200	1,700	1,900	5,900	7,100				
River	8,200	8,200	5,500	5,400	13,700	13,600				
West Bank	4,200	4,500	3,000	1,900	7,200	6,400				
Total (in place)	16,600	17,900	10,200	9,200	26,800	27,100				
Total with 10% Overexcavation			****	· ·	······································					
Factor	18,300	19,700	11,200	10,100	29,500	29,800				

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Attachment C

200-00-00-00-00-00-00-00-00-00-00-00-00-		Sum	mary of HEC-R	AS Predictions 1	for Changes in	Table C-1 Water Surfa	ce Elevations	and Velociti	es for Lyman	St. to Elm St		
				Existing			Design			}		
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB EI, West
500+00		Avg Annual	134	971.69	1,82	134	971.59	1.97	0.15	-0.1	985	985
500+00		0.125-yr	460	973.56	2.55	460	973.43	2.67	0.12	-0.13	985	985
500+00		0.125-yr 0.25-yr	976	975.43	3,25	976	975.27	3.37	0.12	-0.16	985	985
500+00	51948		1422	976.61	3.74	1422	976.48	3.83	0.09	-0.13	985	985
500+00		0.75-yr	1612	977.05	3.92	1612	976.94	4	0.08	-0.11	985	985
500+00	51948		1670	977.18	3.97	1670	977.07	4.05	0.08	-0.11	985	985
500+00	51948		1761	977.38	4.05	1761	977.28	4.12	0.07	-0.1	985	985
500+00	51948		2047	977.97	4.29	2047	977.91	4,33	0.04	-0.06	985	985
500+00	51948		3336	980.31	5.07	3336	980.37	5.03	-0.04	0.06	985	985
500+00	51948	10-vr	4375	981.91	5.53	4375	982.05	5.45	-0.08	0.14	985	985
500+00	51948		7239	986.19	3.56	7239	986.21	3.69	0.13	0.02	985	985
500+00	51948		8721	988.04	2.37	8721	988.02	2.54	0.17	-0.02	985	985
300+00	31340	100-31	0121	300.04	2.01	0,21	000.02				9/4	The state of the s
500+50	51900	Avg Annual	134	971.71	0.89	134	971.62	0.75	-0.14	-0.09	983	984
500+50		0.125-yr	460	973.58	1.73	460	973.47	1,52	-0.21	-0.11	983	984
500+50		0.25-yr	976	975.45	2.48	976	975.32	2.23	-0.25	-0.13	983	984
500+50	51900		1422	976.64	2.95	1422	976.54	2.69	-0.26	-0.1	983	984
500+50		0.75-yr	1612	977.09	3.14	1612	977	2.85	-0.29	-0.09	983	984
500+50	51900		1670	977.22	3.19	1670	977.14	2.9	-0.29	-0.08	983	984
500+50	51900		1761	977.42	3.27	1761	977.35	2.98	-0.29	-0.07	983	984
500+50	51900	2.vr	2047	978.01	3.51	2047	977.98	3.2	-0.31	-0.03	983	984
500+50	51900	5-vr	3336	980.35	4.39	3336	980.45	4	-0.39	0.1	983	984
500+50	51900		4375	981.95	4.93	4375	982.13	4.5	-0.43	0.18	983	984
500+50	51900		7239	985.86	5,43	7239	985.95	5.09	-0.34	0.09	983	984
500+50	51900		8721	987.71	5.2	8721	987.72	4.98	-0.22	0.01	983	984
											22.122	00100
501+00		Avg Annual	134	971.7	0.81	134	971.61	0.93	0.12	-0.09	981.98	984.02
501+00		0.125-yr	460	973.57	1.59	460	973.44	1.82	0.23	-0.13	981.98	984.02
501+00		0.25-уг	976	975.45	2.3	976	975.27	2.62	0.32	-0.18	981.98	984.02
501+00	51850		1422	976.64	2.77	1422	976.48	3.12	0.35	-0.16	981.98	984.02
501+00		0.75-уг	1612	977.08	2.95	1612	976.94	3.31	0.36	-0.14	981.98	984.02
501+00	51850		1670	977.22	3	1670	977.07	3.36	0.36	-0.15	981.98	984.02
501+00	51850		1761	977.41	3.08	1761	977.28	3.44	0.36	-0.13	981.98	984.02
501+00	51850		2047	978.01	3.31	2047	977.9	3.68	0.37	-0.11	981.98	984.02
501+00	51850		3336	980.35	4.14	3336	980.35	4.55	0.41	0	981.98	984.02
501+00	51850		4375	981.97	4.65	4375	982.02	5.09	0.44	0.05	981.98	984.02
501+00	51850		7239	985.88	5.09	7239	985.87	5.59	0.5	-0.01	981.98	984.02
501+00		100-yr	8721	987.72	4.95	8721	987.65	5.45	0.5	-0.07	981.98	984.02
Note:Lymar	St. bridge is lo	cated at Station	499+75. Elm S	t bridge (upstrea	m face) is locate	ed at approxir	natley station	521+68.		0		

						Table C-1		157-110				
		Sum	mary of HEC-R.	AS Predictions 1	for Changes in	water Suna		and Velociti	es for Lyman	St. to Elm Si	L	,
			 	Existing			Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
501+50	51800	Avg Annual	134	971.68	1.25	134	971.6	1.06	-0.19	-0.08	983.55	981
501+50		0.125-yr	460	973.53	2.13	460	973.41	2.01	-0.12	-0.12	983.55	981
501+50	51800	0.25-yr	976	975.38	2.87	976	975.23	2.83	-0.04	-0.15	983.55	981
501+50	51800	0.5-yr	1422	976.56	3.36	1422	976.43	3.34	-0.02	-0.13	983.55	981
501+50	51800	0.75-yr	1612	977	3.55	1612	976.89	3.52	-0.03	-0.11	983,55	981
501+50	51800	1-yr	1670	977.13	3.6	1670	977.03	3.57	-0.03	-0.1	983.55	
501+50	51800	1.5-yr	1761	977.32	3.68	1761	977.23	3.65	-0.03	-0.09	983,55	981
501+50	51800	2-уг	2047	977.91	3.93	2047	977.86	3.88	-0.05	-0.05	983.55	981
501+50	51800	5-yr	3336	980.23	4.8	3336	980.31	4.7	-0.1	0.08	983.55	981
501+50	51800	10-yr	4375	981.84	5.26	4375	982	5.13	-0.13	0.16	983.55	981
501+50	51800		7239	985.86	5.27	7239	985.9	5.26	-0.01	0.04	983.55	981
501+50	51800	100-yr	8721	987.71	5.02	8721	987.68	5.07	0.05	-0.03	983.55	981
502+00	E1750	Avg Annual	134	971.65	1.43	134	971.59	1.05	-0.38	-0.06	981	979
502+00		0.125-yr	460	973.49	2.29	460	973.4	1.89	-0.38	-0.09	981	979
502+00		0.125-yr 0.25-yr	976	975.34	3	976	975.22	2.59	-0.41	-0.12	981	979
502+00	51750		1422	976.52	3.45	1422	976.43	3,02	-0.41	-0.12	981	979
502+00		0.75-yr	1612	976.96	3.62	1612	976.89	3.17	-0.45	-0.07	981	979
502+00	51750		1670	977.09	3.67	1670	977.03	3.22	-0.45	-0.06	981	979
502+00	51750		1761	977.29	3.75	1761	977.24	3.29	-0.46	-0.05	981	979
502+00	51750		2047	977.88	3.98	2047	977.86	3.49	-0.49	-0.02	981	979
502+00	51750		3336	980.2	4.8	3336	980.33	4.2	-0.45	0.13	981	979
502+00	51750		4375	981.83	5.14	4375	982.03	4.53	-0.61	0.2	981	979
502+00	51750		7239	985.89	4.84	7239	985.94	4.61	-0.23	0.05	981	979
502+00	51750		8721	987.74	4.57	8721	987.71	4.49	-0.08	-0.03	981	979
502+50		Avg Annual	134	971.64	1.1	134	971.57	1.1	0	-0.07	979	979
502+50		0.125-yr	460	973.49	1.87	460	973.38	1.92	0.05	-0.11	979	979
502+50		0.25-yr	976	975.34	2.54	976	975.2	2.64	0.1	-0.14	979	979
502+50	51700		1422	976.53	2.98	1422	976.4	3.09	0.11	-0.13	979	979
502+50		0.75-уг	1612	976.97	3.14	1612	976.86	3.25	0.11	-0.11	979	979
502+50	51700		1670	977.1	3,19	1670	977	3.3	0.11	-0.1	979	979
502+50	51700		1761	977.3	3.27	1761	977.21	3,37	0.1	-0.09	979	
502+50	51700		2047	977.89	3,49	2047	977.83	3.58	0.09	-0.06	979	
502+50	51700		3336	980.28	3.77	3336	980.36	3.8	0.03	0.08	979	979
502+50	51700		4375	981.97	3,59	4375	982.12	3.6	0.01	0.15	979	
502+50	51700		7239	986.01	3.11	7239	986.04	3.17	0.06	0.03	979	979
502+50		100-yr	8721	987.83	3.02	8721	987.8	3.09	0.07	-0.03	979	979
Note:Lyman	St. bridge is lo	cated at Station	499+75. Elm S	it bridge (upstrea	m face) is locate	ed at approxir	natley station	521+68.				<u> </u>

		Sum	mary of HEC-R	AS Predictions	for Changes In	Table C-1	ce Elevations	s and Valocit	es for Lyman	St to Elm S		
		Sum	Illiary of nec-ki	Existing	ior changes in	vvater Suria	Design	s and velocit	es for Lyman	OL WEIN S		Î
				LAISTING			Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	ΔEI. (ft)	TOB El. East	TOB El. West
503+00		Avg Annual	134	971.63	0.99	134	971.56	1.2	0.21	-0.07	979.27	979
503+00		0.125-yr	460	973.48	1.56	460	973.36	1.99	0.43	-0.12	979.27	
503+00	51650	0.25-yr	976	975.34	2.09	976	975.17	2,69	0.6	-0.17	979.27	
503+00	51650	0.5-yr	1422	976.54	2.45	1422	976.38	3.13	0.68	-0.16	979.27	
503+00		0.75-yr	1612	976.98	2.59	1612	976.84	3.29	0.7	-0.14	979.27	
503+00	51650	1-yr	1670	977.11	2.63	1670	976.97	3.34	0.71	-0.14	979.27	979
503+00	51650	1.5-yr	1761	977.31	2.69	1761	977.18	3,41	0.72	-0.13	979.27	979
503+00	51650	2-yr	2047	977.91	2.88	2047	977.8	3.62	0.74	-0.11	979.27	979
503+00	51650	5-yr	3336	980.28	3.44	3336	980.28	4.16	0.72	0	979.27	
503+00	51650	10-yr	4375	981.94	3.59	4375	982.03	4.15	0.56	0.09	979.27	979
503+00	51650	50-yr	7239	985.95	3.56	7239	985.96	3.97	0.41	0.01	979.27	979
503+00	51650		8721	987.77	3.57	8721	987.73	3.96	0.39	-0.04	979.27	979
											·	
503+50	51600	Avg Annual	134	971.57	1.69	134	971.51	1.71	0.02	-0,06	978	980,69
503+50		0.125-yr	460	973.41	2.3	460	973.29	2.52	0.22	-0.12	978	
503+50		0.25-yr	976	975.26	2.77	976	975.1	3.08	0.31	-0.16	978	980.69
503+50	51600		1422	976.45	3.09	1422	976.31	3.45	0.36	-0.14	978	980.69
503+50		0.75-yr	1612	976.9	3.21	1612	976.77	3.59	0.38	-0.13	978	980.69
503+50	51600		1670	977.03	3.25	1670	976,91	3.63	0.38	-0.12	978	980,69
503+50	51600		1761	977.23	3.3	1761	977.12	3.7	0.4	-0.11	978	
503+50	51600		2047	977.83	3,45	2047	977.75	3.87	0.42	-0.08	978	
503+50	51600		3336	980.2	3.9	3336	980.24	4.32	0.42	0.04	978	
503+50	51600		4375	981.88	3.91	4375	981.99	4.29	0.38	0.11	978	
503+50	51600		7239	985.94	3.6	7239	985.95	4	0.4	0.01	978	980,69
503+50	51600		8721	987.77	3.52	8721	987.72	3.93	0.41	-0.05	978	
			-									
504+50	51500	Avg Annual	134	971.5	1.33	134	971.42	1.84	0.51	-0.08	982	981.64
504+50		0.125-yr	460	973.35	1.96	460	973.17	2.66	0.7	-0.18	982	
504+50	51500		976	975.21	2.5	976	975.02	3.15	0.65	-0.19	982	981.64
504+50	51500		1422	976.4	2.84	1422	976.24	3.5	0.66	-0.16	982	981.64
504+50	51500		1612	976.85	2.96	1612	976.7	3.64	0.68	-0.15	982	981.64
504+50	51500		1670	976.98	3	1670	976.84	3.68	0.68	-0.14	982	981.64
504+50	51500		1761	977.18	3.05	1761	977.05	3.74	0.69	-0.13	982	981.64
504+50	51500		2047	977.78	3.21	2047	977.68	3.92	0.71	-0.1	982	981.64
504+50	51500	5-vr	3336	980.16	3.75	3336	980.13	4.58	0.83	-0.03	982	981.64
504+50	51500		4375	981,81	4.02	4375	981.83	4.87	0.85	0.02	982	981.64
504+50	51500		7239	985.9	3.72	7239	985.85	4.52	0.8	-0.05	982	
504+50	51500		8721	987.74	3.54	8721	987.65	4.32	0.76	-0.09	982	981.64
			499+75. Elm S						0.76	-0.09	902	301.04

		Sum	mary of HEC-R	AS Predictions	for Changes In	Table C-1	ce Elevations	and Velociti	es for I yman	St to Elm St		THE PARTY OF THE P
		, out of the same	The state of the co-k.	Existing	ior Changes in	vvater Suria	Design	and velociti	es for Lyman	St. to Elm St		

Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB EI. East	TOB El. West
505+00		Avg Annual	134	971.49	0.98	134	971.43	0.93	-0.05	-0.06	982	981
505+00	51450	0.125-yr	460	973.33	1.72	460	973.19	1.79	0.07	-0.14	982	981
505+00		0.25-yr	976	975.19	2.36	976	975.03	2.51	0.15	-0.16	982	981
505+00	51450		1422	976.38	2.75	1422	976.25	2.94	0.19	-0.13	982	981
505+00		0.75-yr	1612	976.83	2.89	1612	976.71	3.09	0.2	-0.12	982	981
505+00	51450		1670	976.96	2.92	1670	976.85	3.14	0.22	-0.11	982	981
505+00	51450		1761	977.16	2.98	1761	977.06	3.21	0.23	-0.1	982	981
505+00	51450		2047	977.76	3.16	2047	977.69	3.4	0.24	-0.07	982	981
505+00	51450		3336	980.14	3.72	3336	980.16	4.03	0.31	0.02	982	981
505+00	51450		4375	981.79	4.01	4375	981.86	4.36	0.35	0.07	982	981
505+00	51450		7239	985.83	4.13	7239	985.81	4.59	0.46	-0.02	982	981
505+00	51450	100-yr	8721	987.67	4.04	8721	987.6	4.53	0.49	-0.07	982	981
505+50	51400	Avg Annual	134	971.46	1.3	134	971.39	1.65	0.35	-0.07	983	981
505+50	51400	0.125-yr	460	973.29	2.04	460	973.12	2.37	0.33	-0.17	983	981
505+50	51400	0.25-yr	976	975.14	2.67	976	974.96	3	0.33	-0.18	983	981
505+50	51400	0.5-vr	1422	976.33	3.07	1422	976.17	3.4	0.33	-0.16	983	981
505+50		0.75-yr	1612	976.77	3.22	1612	976.64	3.54	0.32	-0.13	983	981
505+50	51400	1-vr	1670	976.9	3.26	1670	976.78	3.58	0.32	-0.12	983	981
505+50	51400		1761	977.1	3.33	1761	976.99	3.65	0.32	-0.11	983	981
505+50	51400		2047	977.69	3.52	2047	977.62	3.83	0.31	-0.07	983	981
505+50	51400		3336	980.06	4.17	3336	980.08	4.43	0.26	0.02	983	981
505+50	51400		4375	981.7	4.53	4375	981.79	4.71	0.18	0.09	983	981
505+50	51400		7239	985.76	4.59	7239	985.76	4.87	0.28	0.00	983	981
505+50	51400		8721	987.63	4.4	8721	987.57	4.71	0.20	-0.06	983	981
506+00	51350	Avg Annual	134	971.44	1.22	134	971.37	1.37	0.15	-0.07	982	980
506+00		0.125-yr	460	973.27	1.96	460	973.08	2.48	0.13			
506+00		0.25-yr	976	975.12	2.59		974.89			-0.19	982	980
506+00	51350		1422	976.31	2.98	976		3.32	0.73	-0.23	982	980
506+00		0.75-yr	1612	976.75		1422	976.09	3.79	0.81	-0.22	982	980
506+00	51350				3.12	1612	976.55	3.95	0.83	-0.2	982	980
506+00			1670	976.88	3.16	1670	976.69	4	0.84	-0.19	982	980
506+00	51350		1761	977.08	3.22	1761	976.9	4.07	0.85	-0.18	982	980
506+00	51350		2047	977.68	3.39	2047	977.52	4.28	0.89	-0.16	982	980
506+00	51350		3336	980.05	3.91	3336	980	4.87	0.96	-0.05	982	980
	51350		4375	981.71	4.13	4375	981.71	5.14	1.01	0	982	980
506+00	51350		7239	985.78	4.14	7239	985.76	4.94	0.8	-0.02	982	980
506+00	51350		8721 499+75. Elm St	987.66	3.84	8721	987.58	4.62	0.78	-0.08	982	980

						Table C-1				S El. S.		
		Sum	mary of HEC-R	AS Predictions	for Changes in	Water Surfa		and Velociti	es for Lyman	St. to EIM SI		
			 г	Existing			Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
506+50	51300	Avg Annual	134	971.43	0.99	134	971.35	1.45	0.46	-0.08	982	978
506+50	51300	0.125-yr	460	973.26	1.71	460	973.05	2.42	0.71	-0.21	982	978
506+50		0.25-yr	976	975.12	2.29	976	974.87	3.07	0.78	-0.25	982	978
506+50	51300	0.5-yr	1422	976.3	2.66	1422	976.08	3.48	0.82	-0.22	982	978
506+50		0.75-yr	1612	976.75	2.79	1612	976.54	3.63	0.84	-0.21	982	978
506+50	51300		1670	976.88	2.83	1670	976.68	3.68	0.85	-0.2	982	978
506+50	51300		1761	977.08	2,89	1761	976.89	3.74	0.85	-0.19	982	978
506+50	51300		2047	977.68	3.05	2047	977.52	3.92	0.87	-0.16	982	978
506+50	51300		3336	980.06	3.57	3336	980.01	4.44	0.87	-0.05	982	978
506+50	51300		4375	981.72	3.8	4375	981.74	4.64	0.84	0.02	982	978
506+50	51300		7239	985.8	3.68	7239	985.77	4.49	0.81	-0.03	982	978
506+50		100-yr	8721	987.68	3.38	8721	987.59	4.19	0.81	-0.09	982	978
000.00	01000	100-31	+		0.00							
507+00	51250	Avg Annual	134	971.41	1.17	134	971.34	1.06	-0,11	-0.07	982	978
507+00		0.125-yr	460	973.23	1.91	460	973.05	1.95	0.04	-0.18	982	978
507+00		0.25-yr	976	975.08	2.52	976	974.86	2.68	0.16	-0.22	982	978
507+00	51250		1422	976.26	2.93	1422	976.08	3,13	0.2	-0.18	982	978
507+00		0.75-yr	1612	976.7	3.09	1612	976.54	3.3	0.21	-0.16	982	978
507+00	51250		1670	976.82	3.13	1670	976.68	3.35	0.22	-0.14	982	978
507+00	51250		1761	977.02	3.13	1761	976.89	3.42	0.22	-0.13	982	978
507+00	51250		2047	977.62	3.4	2047	977.52	3.64	0.24	-0.13	982	978
507+00	51250		3336	979.97	4.09	3336	980	4.26	0.17	0.03	982	978
507+00	51250		4375	981.62	4.4	4375	981.74	4.37	-0.03	0.03	982	978
507+00				985.73		7239	985.81	3.75	-0.47	0.12	982	978
	51250		7239		4.22 3.86		987.62	3.45	-0.41	-0.01	982	978
507+00	51250	100-yr	8721	987.63	3.86	8721	987.62	3.45	-0.41	-0.01	962	3/0
507+50	51200	Avg Annual	134	971.4	1	134	971.34	0.67	-0.33	-0.06	982	980
507+50	51200	0.125-yr	460	973.22	1.8	460	973.06	1.16	-0.64	-0.16	982	980
507+50	51200	0.25-yr	976	975.06	2.41	976	974.9	1.59	-0.82	-0.16	982	980
507+50	51200	0.5-yr	1422	976.24	2.78	1422	976.13	1.87	-0.91	-0.11	982	980
507+50	51200	0.75-yr	1612	976.68	2.92	1612	976.6	1.97	-0.95	-0.08	982	980
507+50	51200		1670	976.81	2.96	1670	976.74	2	-0.96	-0.07	982	980
507+50	51200		1761	977.01	3.02	1761	976.96	2.05	-0.97	-0.05	982	980
507+50	51200		2047	977.61	3.2	2047	977.59	2.19	-1.01	-0.02	982	980
507+50	51200		3336	979.98	3.76	3336	980.1	2.67	-1.09	0.12	982	980
507+50	51200	10-vr	4375	981.62	4.11	4375	981.82	2.93	-1.18	0.2	982	980
507+50	51200		7239	985.72	4.09	7239	985.83	3.05	-1.04	0.11	982	980
507+50		100-yr	8721	987.62	3.78	8721	987.63	2.93	-0.85	0.01	982	980
				t bridge (upstrea			natley station	521+68.				

				AS Predictions		Table C-1	as Elevations	and Valaalt	an far I vman	Ct to Elm C		
		Sum	mary of HEC-R	Existing	ior Changes in	vvater Suria	Design	s and velociti	es for Lyman	St. to Elli S		***************************************
				Existing	•		Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	∆ V (fps)	ΔEI. (ft)	TOB EI. East	TOB EI. West
508+00		Avg Annual	134	971.4	0.87	134	971.33	0.85	-0.02	-0.07	982	978
508+00		0.125-yr	460	973.21	1.61	460	973.02	1.76	0.15	-0.19	982	978
508+00		0.25-yr	976	975.05	2.24	976	974.82	2.54	0.3	-0.23	982	978
508+00	51150		1422	976.23	2.63	1422	976.03	2.99	0.36	-0.2	982	978
508+00		0.75-yr	1612	976.67	2.78	1612	976.49	3.15	0.37	-0.18	982	978
508+00	51150		1670	976.8	2.83	1670	976.62	3.2	0.37	-0.18	982	978
508+00	51150		1761	977	2.9	1761	976.83	3.28	0.38	-0.17	982	978
508+00	51150		2047	977.59	3.09	2047	977.46	3.49	0.4	-0.13	982	978
508+00	51150		3336	979.95	3.78	3336	979.9	4.24	0.46	-0.05	982	978
508+00	51150		4375	981.6	4.11	4375	981.6	4.61	0.5	0	982	978
508+00	51150		7239	985.73	3.93	7239	985.67	4.6	0.67	-0.06	982	978
508+00	51150	100-yr	8721	987.63	3.55	8721	987.53	4.24	0.69	-0.1	982	978
508+50	51100	Avg Annual	134	971.39	0.93	134	971.32	0,96	0.03	-0.07	982	978
508+50		0.125-yr	460	973.19	1.65	460	973.01	1.83	0.18	-0.18	982	978
508+50	51100		976	975.03	2.26	976	974.8	2.51	0.25	-0.23	982	978
508+50	51100		1422	976.21	2.64	1422	976.01	2.91	0.27	-0.2	982	978
508+50		0.75-vr	1612	976.65	2.79	1612	976.48	3.06	0.27	-0.17	982	978
508+50	51100		1670	976.78	2.83	1670	976.61	3.11	0.28	-0.17	982	978
508+50	51100		1761	976.98	2.89	1761	976.82	3.17	0.28	-0.16	982	978
508+50	51100		2047	977.58	3.08	2047	977.45	3.36	0.28	-0.13	982	978
508+50	51100		3336	979.93	3.73	3336	979.9	4.03	0.3	-0.03	982	978
508+50	51100		4375	981.58	4.06	4375	981.61	4.36	0.3	0.03	982	978
508+50	51100		7239	985.71	3.92	7239	985.67	4.36	0.44	-0.04	982	978
508+50	51100		8721	987.63	3.43	8721	987.53	4	0.57	-0.1	982	978
509+00	51050	Avg Annual	134	971.38	0.73	134	971.32	0.81	0.08	-0.06	983	977
509+00		0.125-yr	460	973.19	1.47	460	973	1.68	0.21	-0.19	983	977
509+00	51050		976	975.02	2.1	976	974.79	2.36	0.26	-0.23	983	977
509+00	51050		1422	976.2	2.5	1422	976.01	2.76	0.26	-0.19	983	977
509+00	51050		1612	976.65	2.64	1612	976.47	2.91	0.27	-0.18	983	977
509+00	51050		1670	976.77	2.69	1670	976.6	2.95	0.26	-0.17	983	977
509+00	51050		1761	976.97	2.75	1761	976.81	3.02	0.27	-0.16	983	977
509+00	51050		2047	977.57	2.94	2047	977.44	3.21	0.27	-0.13	983	977
509+00	51050		3336	979.93	3.59	3336	979.9	3.85	0.26	-0.03	983	977
509+00	51050		4375	981.59	3.88	4375	981.61	4.13	0.25	0.02	983	977
509+00	51050		7239	985.71	3.81	7239	985.64	4.43	0.62	-0.07	983	977
509+00	51050		8721	987.61	3.48	8721	987.49	4.22	0.74	-0.12	983	977
				t bridge (upstrea					0.14	·V.12	303	011

				AS Predictions		Table C-1	Flavettana	and Valasie	an fast vman	Ct to Elm Ct		
		Sum	mary of HEC-RA	Existing	or Changes in	water Suria	Design	and velociti	es loi Lyman	St. to Eim St		
***************************************				Existing			Design					:
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
509+50		Avg Annual	134	971.37	1.04	134	971.32	0.83	-0.21	-0.05	983	978
509+50		0.125-yr	460	973.15	1.85	460	972.99	1.62	-0.23	-0.16	983	978
509+50		0.25-yr	976	974.97	2.49	976	974.78	2.25	-0.24	-0.19	983	978
509+50	51000		1422	976.15	2.89	1422	976	2.63	-0.26	-0.15	983	978
509+50		0.75-уг	1612	976.59	3.04	1612	976.46	2.76	-0.28	-0.13	983	978
509+50	51000		1670	976.72	3.08	1670	976.59	2.8	-0.28	-0.13	983	978
509+50	51000		1761	976.91	3.15	1761	976.8	2.87	-0.28	-0.11	983	978
509+50	51000		2047	977.51	3.35	2047	977.43	3.05	-0.3	-0.08	983	978
509+50	51000		3336	979.85	4.03	3336	979.9	3.65	-0.38	0.05	983	978
509+50	51000	10-yr	4375	981.52	4.22	4375	981.62	3.87	-0.35	0.1	983	978
509+50	51000	50-yr	7239	985,66	4.19	7239	985.66	4.07	-0.12	0	983	978
509+50	51000	100-yr	8721	987.59	3.69	8721	987.5	3.85	0.16	-0.09	983	978
510+00	50050	Avg Annual	134	971.35	1.1	134	971.3	1.1	0	-0.05	982	978
510+00		0.125-yr	460	973.12	1,95	460	972.95	1.99	0.04	-0.17	982	978
510+00		0.125-yr 0.25-yr	976	974.93	2.66	976	974.73	2.69	0.03	-0.2	982	978
510+00	50950		1422	976.1	3.09	1422	975.93	3.1	0.03	-0.17	982	978
510+00		0.75-yr	1612	976.54	3.24	1612	976.39	3.25	0.01	-0.15	982	978
510+00	50950		1670	976.67	3.29	1670	976.52	3.29	0.01	-0.15	982	978
510+00	50950		1761	976.86	3.36	1761	976.73	3,36	0	-0.13	982	978
510+00	50950		2047	977.45	3.55	2047	977.35	3.56	0,01	-0.1	982	978
510+00	50950		3336	979.8	4.22	3336	979.81	4.2	-0.02	0.01	982	978
510+00	50950		4375	981.48	4.4	4375	981.53	4.45	0.05	0.05	982	978
510+00	50950		7239	985.64	4.26	7239	985.59	4.55	0.29	-0.05	982	978
510+00		100-yr	8721	987.56	3.93	8721	987.45	4.32	0.39	-0.11	982	978
510+50		Avg Annual	134	971.32	1.32	134	971.29	1.05	-0.27	-0.03	982	978
510+50		0.125-yr	460	973.06	2.32	460	972.93	1.92	-0.4	-0.13	982	978
510+50		0.25-yr	976	974.85	3.07	976	974.71	2.63	-0.44	-0.14	982	978
510+50	50900		1422	976.02	3.52	1422	975.91	3.05	-0.47	-0.11	982	978
510+50		0.75-yr	1612	976.45	3.69	1612	976.37	3.2	-0.49	-0.08	982	978
510+50	50900		1670	976.58	3.74	1670	976.5	3.24	-0.5	-0.08	982	978
510+50	50900	1.5-yr	1761	976.77	3.81	1761	976.71	3.31	-0.5	-0.06	982	978
510+50	50900		2047	977.35	4.04	2047	977.34	3.51	-0.53	-0.01	982	978
510+50	50900		3336	979.67	4.86	3336	979.79	4.16	-0.7	0.12	982	978
510+50	50900	10-yr	4375	981.35	5.03	4375	981.51	4,39	-0.64	0.16	982	978
510+50	50900	50-yr	7239	985.52	5	7239	985.58	4.54	-0.46	0.06	982	978
510+50		100-yr	8721	987.46	4.71	8721	987.43	4.41	-0.3	-0.03	982	978
Note:Lyman	St. bridge is lo	cated at Station	499+75. Elm S	t bridge (upstrea	m face) is locate	ed at approxin	natley station	521+68.				

				AS Predictions	for Changes In	Table C-1	ce Elevations	and Velociti	es for Lyman	St to Flm St		
		Sum	mary of HEC-R	····	for Changes in	Water Suria	Design	and velocit	es for Eyman	OE to Lim o		
······································				Existing			Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	∆ V (fps)	Δ El. (ft)	TOB El. East	TOB El. West
511+00		Avg Annual	134	971.31	1.01	134	971.28	0.92	-0.09	-0.03	984	978
511+00		0.125-yr	460	973.05	1.93	460	972.92	1.92	-0.01	-0.13	984	978
511+00		0.25-yr	976	974.83	2.65	976	974.67	2.74	0.09	-0.16	984	978
511+00	50850		1422	976	3.06	1422	975.87	3.21	0.15	-0.13	984	978
511+00		0.75-yr	1612	976.44	3.22	1612	976.33	3.38	0.16	-0.11	984	978
511+00	50850		1670	976,56	3.26	1670	976.46	3,43	0.17	-0.1	984	978
511+00	50850		1761	976.76	3.33	1761	976.67	3.5	0.17	-0.09	984	978
511+00	50850		2047	977.35	3.53	2047	977.29	3.72	0.19	-0.06	984	978
511+00	50850		3336	979.71	4.03	3336	979.77	4.21	0.18	0.06	984	978
511+00	50850		4375	981.4	4.15	4375	981.51	4.38	0.23	0.11	984	978
511+00	50850		7239	985.58	4.05	7239	985.57	4.63	0.58	-0.01	984	978
511+00	50850		8721	987.5	3,83	8721	987.41	4.56	0.73	-0.09	984	978
311100	00000	100-71										<u> </u>
511+50	50800	Avg Annual	134	971.3	1.03	134	971.27	1.14	0.11	-0.03	981	980
511+50		0.125-yr	460	973.02	1.86	460	972.89	2.08	0.22	-0.13	981	980
511+50		0.25-yr	976	974.8	2.54	976	974.64	2.82	0.28	-0.16	981	980
511+50	50800		1422	975.97	2.96	1422	975.84	3.26	0.3	-0.13	981	980
511+50		0.75-yr	1612	976.4	3.12	1612	976,3	3.42	0.3	-0.1	981	980
511+50	50800		1670	976.53	3.17	1670	976.43	3.47	0.3	-0.1	981	980
511+50	50800		1761	976.72	3.24	1761	976.64	3.54	0.3	-0.08	981	980
511+50	50800		2047	977.31	3.45	2047	977.26	3.75	0.3	-0.05	981	980
511+50	50800		3336	979.63	4.19	3336	979.69	4.49	0.3	0.06	981	980
511+50	50800		4375	981.3	4,13	4375	981.41	4.77	0.26	0.11	981	980
			7239	985.47	4.59	7239	985.49	4.94	0.35	0.02	981	
511+50	50800		8721	987.41	4.36	8721	987.35	4.8	0.33	-0.06	981	980
511+50	50800	100-yr	8/21	987.41	4.36	0/21	967.33	4.0	0.44	-0.00		
512+00	50750	Avg Annual	134	971.28	1.05	134	971.26	1.02	-0.03	-0.02	981	979
512+00		0.125-yr	460	972.99	1.88	460	972.87	2.01	0.13	-0.12	981	979
512+00		0.25-yr	976	974.76	2.59	976	974.62	2.81	0.22	-0.14	981	979
512+00	50750		1422	975.92	3.03	1422	975.81	3.29	0.26	-0.11	981	979
512+00		0.75-yr	1612	976.35	3.2	1612	976.26	3.46	0.26	-0.09	981	979
512+00	50750		1670	976.48	3.25	1670	976.4	3.51	0.26	-0.08	981	979
512+00	50750		1761	976.68	3.33	1761	976.6	3.59	0.26	-0.08	981	
512+00	50750		2047	977.26	3.55	2047	977.22	3.82	0.27	-0.04	981	
512+00	50750		3336	979.57	4.35	3336	979.64	4.65	0.3	0.07	981	979
512+00	50750		4375	981.21	4.8	4375	981.32	5.08	0.28	0.11	981	979
512+00	50750		7239	985.44	4.69	7239	985.43	5.21	0.52	-0.01	981	979
512+00	50750		8721	987.4	4.35	8721	987.32	4.97	0.62	-0.08	981	979
				987.4 St bridge (upstrea					0.02	-0.08		

		Sum	mary of HEC-R	AS Predictions t	for Changes in	Table C-1 Water Surfa	ce Elevations	and Velocit	es for Lyman	St. to Elm Si		page-10-10-10-10-10-10-10-10-10-10-10-10-10-
				Existing			Design					
Station	Rvr, Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
512+50		Avg Annual	134	971.27	0.89	134	971.24	1.36	0.47	-0.03	980	982.12
512+50		0,125-yr	460	972.97	1.81	460	972.81	2.46	0.65	-0.16	980	982.12
512+50		0.25-yr	976	974.73	2.56	976	974.55	3.17	0.61	-0.18	980	982.12
512+50	50700		1422	975.89	3.01	1422	975.74	3.6	0.59	-0.15	980	982.12
512+50		0.75-yr	1612	976.32	3.18	1612	976.2	3.75	0.57	-0.12	980	982.12
512+50	50700		1670	976.45	3.23	1670	976.33	3.79	0.56	-0.12	980	982.12
512+50	50700		1761	976.65	3.3	1761	976.54	3.86	0.56	-0.11	980	982.12
512+50	50700		2047	977.23	3.53	2047	977.16	4.05	0.52	-0.07	980	982.12
512+50	50700		3336	979.54	4.28	3336	979.6	4.74	0.46	0.06	980	982.12
512+50	50700		4375	981.19	4.73	4375	981.3	5.1	0.37	0.11	980	982.12
512+50	50700	50-vr	7239	985.34	5.05	7239	985.36	5.49	0.44	0.02	980	
512+50		100-yr	8721	987.29	4.93	8721	987.22	5.43	0.5	-0.07	980	982.12
513+00	50650	Avg Annual	134	971.27	0.76	134	971.24	0.79	0.03	-0.03	983	982.66
513+00		0.125-yr	460	972.95	1.65	460	972.82	1.74	0.09	-0.13	983	982.66
513+00	50650	0.25-yr	976	974.71	2.45	976	974.56	2.57	0.12	-0.15	983	982.66
513+00	50650		1422	975.86	2.95	1422	975.75	3.06	0.11	-0.11	983	982.66
513+00	50650	0.75-yr	1612	976.3	3.14	1612	976.21	3.24	0.1	-0.09	983	982.66
513+00	50650	1-yr	1670	976.42	3.19	1670	976.34	3.3	0.11	-0.08	983	982.66
513+00	50650	1.5-yr	1761	976.62	3.27	1761	976.55	3.38	0.11	-0.07	983	982.66
513+00	50650	2-yr	2047	977.2	3.5	2047	977.17	3.61	0.11	-0.03	983	982.66
513+00	50650	5-yr	3336	979.52	4.27	3336	979.61	4.4	0.13	0.09	983	982.66
513+00	50650	10-yr	4375	981.15	4.77	4375	981.29	4.85	0.08	0.14	983	982.66
513+00	50650	50-уг	7239	985.32	5.15	7239	985.35	5.33	0.18	0.03	983	982.66
513+00	50650	100-уг	8721	987.28	4.91	8721	987.22	5.24	0.33	-0.06	983	982.66
513+50	50600	Avg Annual	134	971.25	0.88	134	971.23	1.06	0.18	-0.02	982	981
513+50	50600	0.125-yr	460	972.92	1.77	460	972.78	2.05	0.28	-0.14	982	981
513+50	50600	0.25-yr	976	974.68	2.47	976	974.52	2.75	0.28	-0.16	982	981
513+50	50600	0.5-yr	1422	975.83	2.87	1422	975.72	3.11	0.24	-0.11	982	981
513+50	50600	0.75-yr	1612	976.27	3.02	1612	976.19	3.24	0.22	-0.08	982	981
513+50	50600	1-yr	1670	976.39	3.07	1670	976.32	3.28	0.21	-0.07	982	981
513+50	50600		1761	976.59	3.13	1761	976.53	3.34	0.21	-0.06	982	981
513+50	50600		2047	977.17	3.33	2047	977.15	3.52	0.19	-0.02	982	981
513+50	50600	5-yr	3336	979.49	4.02	3336	979.61	4.15	0,13	0.12	982	981
513+50	50600		4375	981.13	4.46	4375	981.3	4.52	0.06	0.17	982	981
513+50	50600		7239	985,34	4.53	7239	985.39	4.71	0.18	0.05	982	981
513+50		100-yr	8721	987.3	4.29	8721	987.26	4.6	0.31	-0.04	982	981
Note:Lymai	St. bridge is lo	cated at Station	1 499+75. Elm S	st bridge (upstrea	m face) is locate	ed at approxir	natley station	521+68.				

		Sum	mary of HEC-R	AS Predictions t	or Changes In	Table C-1 Water Surfa	ce Elevations	and Velociti	es for Lyman	St. to Elm St		
			1	Existing	1		Design					
Station	Rvr. Sta.	Profile	Q (cfs)	EI. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
514+00		Avg Annual	134	971.24	0.92	134	971,23	0.65	-0.27	-0.01	984.1	981
514+00		0.125-yr	460	972.89	1,9	460	972.79	1.44	-0.46	-0.1	984.1	981
514+00		0.25-yr	976	974.62	2.72	976	974.53	2.12	-0.6	-0.09	984.1	981
514+00	50550		1422	975.77	3.22	1422	975.74	2.54	-0.68	-0.03	984.1	981
514+00		0.75-yr	1612	976.19	3,4	1612	976.2	2.7	-0.7	0.01	984.1	981
514+00	50550		1670	976.32	3.45	1670	976.33	2.74	-0.71	0.01	984.1	981
514+00	50550		1761	976.51	3,53	1761	976.54	2.81	-0.72	0.03	984.1	981
514+00	50550		2047	977.09	3.77	2047	977.17	3	-0.77	0.08	984.1	981
514+00	50550		3336	979.39	4.53	3336	979.62	3.7	-0.83	0.23	984.1	981
514+00	50550	10-vr	4375	981.08	4.8	4375	981.33	4.01	-0.79	0.25	984.1	981
514+00	50550		7239	985.42	3.66	7239	985.51	3.27	-0.39	0.09	984.1	981
514+00		100-yr	8721	987.4	2.79	8721	987.39	2.65	-0.14	-0.01	984.1	981
514+50	50500	Avg Annual	134	971.24	0.89	134	971.22	0.93	0.04	-0.02	986.7	981
514+50		0.125-yr	460	972.87	1.86	460	972.74	1.99	0.13	-0.13	986.7	981
514+50		0.25-yr	976	974.59	2.66	976	974.45	2.85	0.19	-0.14	986.7	981
514+50		0.5-yr	1422	975.73	3.14	1422	975.63	3.33	0.19	-0.1	986.7	981
514+50		0.75-yr	1612	976.16	3.32	1612	976.08	3.5	0.18	-0.08	986.7	981
514+50	50500		1670	976.29	3.37	1670	976,22	3.55	0.18	-0.07	986.7	981
514+50		1.5-yr	1761	976.48	3.45	1761	976.42	3.62	0.17	-0.06	986.7	981
514+50	50500		2047	977.06	3.69	2047	977.04	3.83	0.14	-0.02	986.7	981
514+50	50500	5-vr	3336	979.36	4.47	3336	979.47	4.5	0.03	0.11	986.7	981
514+50	50500		4375	981.03	4.8	4375	981.19	4.68	-0.12	0.16	986.7	981
514+50	50500	50-yr	7239	985.39	3.74	7239	985.49	3.26	-0.48	0.1	986.7	981
514+50		100-yr	8721	987.39	2.85	8721	987.38	2.52	-0.33	-0.01	986.7	981
515+00	50450	Avg Annual	134	971.22	1.12	134	971.21	0.86	-0.26	-0.01	986.87	981
515+00	50450	0.125-yr	460	972.83	2.11	460	972.72	1.93	-0.18	-0.11	986.87	981
515+00	50450	0.25-yr	976	974.53	2.9	976	974,41	2.85	-0.05	-0.12	986.87	981
515+00		0.5-yr	1422	975.67	3.38	1422	975.58	3.38	0	-0.09	986.87	981
515+00	50450	0.75-yr	1612	976.09	3.56	1612	976.03	3,56	0	-0.06	986.87	981
515+00	50450	1-yr	1670	976.22	3.61	1670	976.16	3.62	0.01	-0.06	986,87	981
515+00		1.5-yr	1761	976.41	3.69	1761	976.37	3.69	0	-0.04	986,87	981
515+00	50450	2-yr	2047	976.98	3.93	2047	976.98	3.92	-0.01	0	986.87	981
515+00	50450		3336	979.27	4.73	3336	979.39	4.74	0.01	0.12	986.87	981
515+00	50450		4375	980.94	5.09	4375	981.08	5.13	0.04	0.14	986.87	981
515+00	50450	50-yr	7239	985.24	4.68	7239	985.31	4.71	0.03	0.07	986.87	981
515+00		100-yr	8721	987.31	3.66	8721	987.29	3.72	0.06	-0.02	986,87	981
Note:Lyma	n St. bridge is lo	cated at Station	499+75. Elm S	t bridge (upstrea	m face) is locate	ed at approxir	natley station	521+68.				

		Sum	mary of HEC-R	AS Predictions 1	for Changes in	Table C-1 Water Surfa	ce Elevations	and Velociti	es for Lyman	St, to Elm St		
				Existing	<u> </u>		Design		.,			
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
515+50		Avg Annual	134	971.21	0.82	134	971.21	0.65	-0.17	0	987	980
515+50		0.125-yr	460	972.82	1.74	460	972.72	1.54	-0.2	-0.1	987	980
515+50		0.25-yr	976	974.52	2.56	976	974.42	2.35	-0.21	-0.1	987	980
515+50	50400		1422	975,66	3.07	1422	975.59	2.83	-0.24	-0.07	987	980
515+50		0.75-yr	1612	976.08	3.26	1612	976.04	3	-0.26	-0.04	987	980
515+50	50400		1670	976.2	3,31	1670	976,17	3.05	-0.26	-0.03	987	980
515+50	50400		1761	976,39	3.4	1761	976.38	3,12	-0.28	-0.01	987	980
515+50	50400		2047	976.97	3.65	2047	976.99	3.33	-0.32	0.02	987	980
515+50	50400		3336	979.25	4,53	3336	979.42	4.03	-0.5	0.17	987	980
515+50	50400		4375	980.9	5.03	4375	981.11	4.41	-0.62	0.21	987	980
515+50	50400		7239	985.06	5.45	7239	985.28	4.43	-1.02	0.22	987	980
515+50	50400		8721	987.12	4.93	8721	987.2	4.08	-0.85	0.08	987	980
516+00	50350	Avg Annual	134	971.2	0.95	134	971.21	0.64	-0.31	0.01	989	981
516+00		0.125-yr	460	972.79	1.94	460	972.71	1,54	-0.4	-0.08	989	981
516+00		0.25-yr	976	974.47	2.75	976	974.39	2.37	-0.38	-0.08	989	981
516+00	50350		1422	975,61	3.21	1422	975.56	2.86	-0.35	-0.05	989	981
516+00		0.75-yr	1612	976.03	3.39	1612	976.01	3.03	-0.36	-0.02	989	981
516+00	50350		1670	976.15	3.44	1670	976.14	3.08	-0.36	-0.01	989	981
516+00	50350		1761	976,35	3.51	1761	976.35	3.15	-0.36	0	989	981
516+00	50350		2047	976.92	3.74	2047	976.96	3.37	-0.37	0.04	989	981
516+00	50350		3336	979.21	4.54	3336	979.37	4.08	-0.46	0.16	989	981
516+00	50350		4375	980.86	5.02	4375	981.06	4.48	-0.54	0.2	989	981
516+00	50350		7239	985.03	5.41	7239	985.18	4.83	-0.58	0.15	989	981
516+00	50350		8721	987.12	4.76	8721	987.15	4.31	-0.45	0.03	989	981
516+50		Avg Annual	134	971.2	0.88	134	971.21	0.68	-0.2	0.01	990.05	982
516+50	50300	0.125-yr	460	972.76	1.98	460	972.69	1.68	-0.3	-0.07	990.05	982
516+50	50300	0.25-yr	976	974.42	2.95	976	974.35	2.62	-0.33	-0.07	990.05	982
516+50	50300		1422	975.53	3.52	1422	975.5	3.18	-0.34	-0.03	990.05	982
516+50	50300	0.75-yr	1612	975.94	3.74	1612	975.94	3,38	-0.36	0	990.05	982
516+50	50300	1-yr	1670	976.07	3.8	1670	976.07	3.43	-0.37	0	990.05	982
516+50	50300	1.5-yr	1761	976.26	3.89	1761	976.27	3,52	-0.37	0.01	990.05	982
516+50	50300		2047	976.82	4.17	2047	976.88	3.76	-0.41	0.06	990.05	982
516+50	50300	5-yr	3336	979.07	5.15	3336	979.26	4.56	-0.59	0.19	990.05	982
516+50	50300	10-уг	4375	980.69	5.71	4375	980.93	5	-0.71	0.24	990.05	982
516+50	50300		7239	984.73	6.65	7239	984.98	5.67	-0.98	0.25	990.05	982
516+50	50300	100-yr	8721	986.79	6.38	8721	986.94	5.42	-0.96	0.15	990.05	982
Note:Lymar			499+75. Elm S	t bridge (upstrea	m face) is locate	ed at approxin	natley station	521+68.	***************************************			

		Sum	many of HEC-R	AS Predictions	for Changes in	Table C-1 Water Surfa	ce Elevations	and Velociti	es for Lyman	St. to Elm St		
			linary or neo-no	Existing			Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
517+00		Avg Annual	134	971.19	0,85	134	971.21	0.66	-0.19	0.02	989.9	983
517+00		0.125-yr	460	972.74	1,97	460	972.68	1.67	-0.3	-0.06	989.9	983
517+00		0.25-yr	976	974,37	3.03	976	974.32	2.67	-0.36	-0.05	989.9	983
517+00	50250		1422	975.47	3.68	1422	975.46	3.26	-0.42	-0.01	989.9	983
517+00		0.75-yr	1612	975.87	3.92	1612	975.9	3.47	-0.45	0.03	989.9	983
517+00	50250		1670	976	4	1670	976.03	3,53	-0.47	0.03	989.9	983
517+00	50250		1761	976.18	4.1	1761	976.22	3.62	-0.48	0.04	989.9	983
517+00	50250		2047	976.73	4.42	2047	976.82	3.89	-0.53	0.09	989.9	983
517+00	50250		3336	978.95	5.53	3336	979.18	4.76	-0.77	0.23	989,9	983
517+00	50250		4375	980.55	6.17	4375	980.84	5.27	-0.9	0.29	989.9	983
517+00	50250		7239	984.67	6.89	7239	984.86	6.11	-0.78	0.19	989.9	983
517+00		100-yr	8721	986.82	6.16	8721	986.86	5.76	-0.4	0.04	989,9	983
517+50	50200	Avg Annual	134	971.18	0.86	134	971.2	0.72	-0.14	0.02	989.59	983
517+50		0.125-yr	460	972.72	1.9	460	972.66	1.79	-0.11	-0.06	989.59	983
517+50		0.25-yr	976	974.35	2.85	976	974.28	2.84	-0.01	-0.07	989,59	983
517+50	50200		1422	975.44	3.42	1422	975.4	3.46	0.04	-0.04	989.59	983
517+50		0.75-yr	1612	975.85	3.64	1612	975.83	3.68	0.04	-0.02	989.59	983
517+50	50200		1670	975.98	3.7	1670	975.96	3.75	0.05	-0.02	989.59	983
517+50	50200		1761	976.16	3.8	1761	976.16	3.84	0.04	0	989.59	983
517+50	50200		2047	976.72	4.08	2047	976.74	4.12	0.04	0.02	989,59	983
517+50	50200		3336	978.95	5.06	3336	979.09	5.01	-0.05	0.14	989.59	983
517+50	50200		4375	980.56	5.63	4375	980.75	5.48	-0.15	0.19	989.59	983
517+50	50200		7239	984.65	6.56	7239	984.78	6.17	-0.39	0.13	989.59	983
517+50		100-yr	8721	986.59	6.71	8721	986.72	6.07	-0.64	0.13	989.59	983
518+00	50150	Avg Annual	134	971.18	0.85	134	971.2	0.62	-0.23	0.02	990	984
518+00	50150	0.125-yr	460	972.7	1.84	460	972.66	1.55	-0.29	-0.04	990	984
518+00	50150	0.25-yr	976	974.32	2.74	976	974.28	2.49	-0.25	-0.04	990	984
518+00	50150	0.5-yr	1422	975.41	3.29	1422	975.4	3.05	-0.24	-0.01	990	984
518+00	50150	0.75-yr	1612	975.83	3.49	1612	975.83	3.26	-0.23	0	990	984
518+00	50150	1-yr	1670	975.95	3,55	1670	975.96	3.31	-0.24	0.01	990	984
518+00	50150		1761	976.13	3.64	1761	976.15	3.4	-0.24	0.02	990	984
518+00	50150		2047	976,69	3.91	2047	976.74	3.66	-0.25	0.05	990	984
518+00	50150		3336	978.93	4.84	3336	979.09	4.55	-0.29	0.16	990	984
518+00	50150		4375	980.55	5.38	4375	980.75	5.08	-0.3	0.2	990	984
518+00	50150		7239	984.62	6.39	7239	984.76	6.07	-0.32	0.14	990	984
518+00		100-yr	8721	986.59	6.45	8721	986.68	6.18	-0.27	0.09	990	984
Note:Lyma	n St. bridge is lo	cated at Station	499+75. Elm S	t bridge (upstrea	m face) is locate	ed at approxir	natley station	521+68.				

			mary of HEC-R	AC Desdistance		Table C-1	as Elevations	and Valaciti	or for Lymps	Ct to Elm Ct		
		Sum	mary of HEC-K		for Changes in	vvater Suria		and velocid	es for Lyman	St. to Elli St		
				Existing			Design					
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	∆ V (fps)	Δ El. (ft)	TOB El. East	TOB El. West
518+50	50100	Avg Annual	134	971.17	0.78	134	971.2	0.58	-0.2	0.03	988	983
518+50		0.125-yr	460	972.69	1.68	460	972.66	1.44	-0.24	-0.03	988	983
518+50		0.25-yr	976	974.31	2.48	976	974.27	2.26	-0.22	-0.04	988	983
518+50	50100	0.5-yr	1422	975.4	2.94	1422	975.39	2.76	-0.18	-0.01	988	983
518+50	50100	0.75-yr	1612	975.82	3,11	1612	975.83	2.93	-0.18	0.01	988	983
518+50	50100	1-yr	1670	975.94	3.16	1670	975.95	2.98	-0.18	0.01	988	983
518+50	50100		1761	976.13	3.23	1761	976.15	3.06	-0.17	0.02	988	983
518+50	50100	2-yr	2047	976.69	3.45	2047	976.74	3.28	-0.17	0.05	988	983
518+50	50100		3336	978.95	4.21	3336	979.1	4.07	-0.14	0.15	988	983
518+50	50100	10-yr	4375	980.59	4.64	4375	980.77	4.54	-0.1	0.18	988	983
518+50	50100	50-yr	7239	984,71	5.38	7239	984.81	5.43	0.05	0.1	988	983
518+50		100-yr	8721	986.67	5.49	8721	986,71	5.62	0.13	0.04	988	983
519+00	50050	Avg Annual	134	971.15	1.13	134	971.19	0.78	-0.35	0.04	984.56	986
519+00		0.125-yr	460	972.63	2.29	460	972.63	1,75	-0.54	0	984.56	986
519+00		0.25-yr	976	974.2	3.24	976	974.22	2.6	-0.64	0.02	984.56	986
519+00	50050		1422	975.27	3.77	1422	975.33	3.09	-0.68	0.06	984.56	986
519+00		0.75-yr	1612	975.67	3.96	1612	975.76	3.26	-0,7	0.09	984.56	986
519+00	50050		1670	975.79	4.02	1670	975.89	3.31	-0.71	0.1	984.56	986
519+00	50050	1.5-vr	1761	975.97	4.1	1761	976.08	3.38	-0.72	0.11	984.56	986
519+00	50050	2-vr	2047	976.53	4.34	2047	976.67	3.59	-0.75	0.14	984.56	986
519+00	50050		3336	978.75	5.16	3336	979.03	4.34	-0.82	0.28	984.56	986
519+00	50050		4375	980.38	5.6	4375	980.7	4.79	-0.81	0.32	984.56	986
519+00	50050	50-vr	7239	984.48	6.38	7239	984.73	5.66	-0.72	0.25	984.56	986
519+00	50050	100-yr	8721	986.39	6.68	8721	986.63	5.9	-0.78	0.24	984.56	986
519+50	50000	Avg Annual	134	971.11	1.58	134	971.18	0.91	-0.67	0.07	985.1	986
519+50	50000	0.125-yr	460	972.51	2.92	460	972.57	2	-0.92	0.06	985.1	986
519+50		0.25-yr	976	974.04	3.91	976	974.12	2.93	-0.98	0.08	985.1	986
519+50	50000		1422	975.1	4.44	1422	975.21	3.45	-0.99	0.11	985.1	986
519+50		0.75-yr	1612	975.5	4.64	1612	975.64	3.63	-1.01	0.14	985.1	986
519+50	50000		1670	975.61	4.7	1670	975.76	3.68	-1.02	0.15	985.1	986
519+50	50000		1761	975.8	4.78	1761	975.95	3.76	-1.02	0.15	985.1	986
519+50	50000		2047	976.34	5.04	2047	976.54	3.98	-1.06	0.2	985.1	986
519+50	50000		3336	978.56	5.88	3336	978.89	4.66	-1.22	0.33	985.1	986
519+50	50000		4975	980,19	6.3	4375	980.57	5.01	-1.29	0.38	985.1	986
519+50	50000		7239	984.35	6.91	7239	984,65	5.52	-1.39	0.3	985.1	986
519+50		100-yr	8721	986.28	7.13	8721	986.56	5.66	-1.47	0.28	985.1	986
			499+75. Elm S									

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	-		 	Existing		T	Design		i			
Station	Rvr. Sta.	Profile	Q (cfs)	El. (ft.)	V (fps)	Q (cfs)	El. (ft)	V (fps)	ΔV (fps)	Δ El. (ft)	TOB El. East	TOB El. West
520+00	49950	Avg Annual	134	971.09	1.28	134	971.16	0.98	-0.3	0.07	987.01	988
520+00		0.125-yr	460	972.47	2.58	460	972.52	2.2	-0.38	0.05	987.01	988
520+00		0.25-yr	976	973.98	3.64	976	974.04	3.29	-0.35	0.06	987.01	988
520+00	49950		1422	975.03	4.24	1422	975.1	3.93	-0.31	0.07	987.01	988
520+00		0.75-yr	1612	975.43	4.45	1612	975.51	4.14	-0,31	0.08	987.01	988
520+00	49950	1-vr	1670	975.55	4.51	1670	975.63	4.21	-0.3	0.08	987.01	988
520+00	49950		1761	975.73	4.61	1761	975.81	4.3	-0.31	0.08	987.01	988
520+00	49950		2047	976.27	4.89	2047	976.38	4.57	-0.32	0.11	987.01	988
520+00	49950		3336	978.48	5.87	3336	978.68	5.4	-0.47	0.2	987.01	988
520+00	49950		4375	980.08	6.42	4375	980.34	5.77	-0.65	0.26	987.01	988
520+00	49950		7239	984.16	7,361	7239	984.4	6.43	-0.93	0.24	987.01	988
520+00	49950		8721	986.06	7.7	8721	986.28	6.7	-1	0.22	987.01	988
		,										
520+50	49900	Avg Annual	134	971.08	0.93	134	971.15	0.95	0.02	0.07	988	989
520+50		0.125-yr	460	972.46	2.02	460	972.49	2.18	0.16	0.03	988	989
520+50		0.25-yr	976	973.98	2.98	976	973.97	3.31	0.33	-0.01	988	989
520+50	49900		1422	975.03	3.53	1422	975.02	3.98	0.45	-0.01	988	989
520+50		0.75-yr	1612	975,43	3.73	1612	975.42	4.2	0.47	-0.01	988	989
520+50	49900		1670	975.55	3.78	1670	975.54	4.27	0.49	-0.01	988	989
520+50	49900		1761	975,74	3.87	1761	975.72	4.37	0.5	-0.02	988	989
520+50	49900	2-yr	2047	976.29	4.12	2047	976.29	4.65	0.53	0	988	989
520+50	49900		3336	978.51	5	3336	978.55	5.54	0.54	0.04	988	989
520+50	49900		4375	980.14	5.51	4375	980.18	6	0.49	0.04	988	989
520+50	49900		7239	984.24	6.4	7239	984.25	6.63	0.23	0.01	988	989
520+50	49900		8721	986.15	6.73	8721	986.15	6.79	0.06	0	988	989
521+00	49850	Avg Annual	134	971.06	1.18	134	971.13	1.1	-0.08	0.07	988	990
521+00		0.125-yr	460	972.39	2.42	460	972.42	2.43	0.01	0.03	988	990
521+00		0.25-yr	976	973.87	3.45	976	973.87	3.6	0.15	0	988	990
521+00	49850		1422	974.9	4.04	1422	974.89	4,27	0.23	-0.01	988	990
521+00		0.75-yr	1612	975.3	4.25	1612	975.29	4.51	0.26	-0.01	988	990
521+00	49850		1670	975.41	4.31	1670	975.41	4,57	0.26	0	988	990
521+00	49850		1761	975.59	4.4	1761	975.59	4.67	0.27	0	988	990
521+00	49850		2047	976.14	4.65	2047	976.14	4.95	0.3	0	988	990
521+00	49850		3336	978.35	5.55	3336	978.38	5.83	0.28	0.03	988	990
521+00	49850		4375	979.96	6.06	4375	980	6.26	0.2	0.04	988	990
521+00	49850		7239	984.06	6.95	7239	984.07	6.94	-0.01	0.01	988	990
521+00	49850		8721	985.97	7.28	8721	985.95	7.21	-0.07	-0.02	988	990















